

# The characteristics of high strength and lead-free machinable $\alpha$ - $\beta$ duplex phase brass Cu-40Zn-Cr-Fe-Sn-Bi alloy

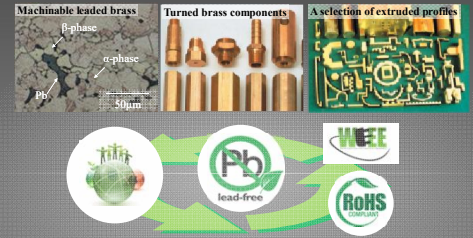


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## Introduction

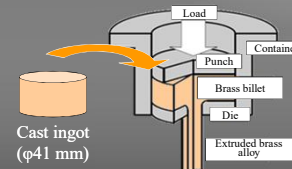
**Brass alloys** are used for pipes, valves, and fittings in systems that transport water and other aqueous fluids because of their excellent corrosion resistance. **Pb** at levels of 2-5 mass% is also added to traditional brasses to improve their machinability. However, addition of **Pb** to these materials is a significant, severe **hazard** to the environment and human health. Thus, material designs must consider safety according to the regulations of the Restriction of Hazardous Substance (RoHS) and Waste Electrical and Electronic Equipment (WEEE) Directives. **New high-strength, Pb-free machinable  $\alpha$ - $\beta$  duplex brass alloys with dispersed Bi particles** were produced using a **casting** and **extrusion** process. The effects of **Bi dispersoids** on the mechanical properties and machinability of the extruded specimens were investigated.



## Materials and methods

Alloys	Sn	Pb	Zn	Fe	Cr	Bi	Cu	Vickers micro hardness / Hv0.025	
								$\alpha$ -phase	$\beta$ -phase
CAST1	0.59	-0.005	40.86	0.22	0.34	---	Bal.	110	170
CAST2	0.595	-0.005	40.81	0.229	0.256	0.994	Bal.	108	165
CAST3	0.6	-0.005	40.64	0.23	0.26	2.02	Bal.	111	168
CAST4	0.578	-0.005	40.83	0.219	0.22	2.85	Bal.	112	169

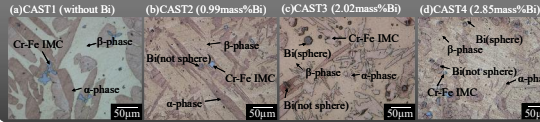
Cu-40Zn alloy  
 $\alpha$ -phase: 100 Hv  
 $\beta$ -phase: 144 Hv



### Hot extrusion

2000 kN hydraulic direct press machine  
 Extrusion speed: 3 mm/s  
 Diameter of extruded specimen: 7 mm  
 Pre-heating conditions: 923 K for 180 s in Ar gas atmosphere

The extruded CAST1-4 specimens are denoted as EXT1-4 in this study.

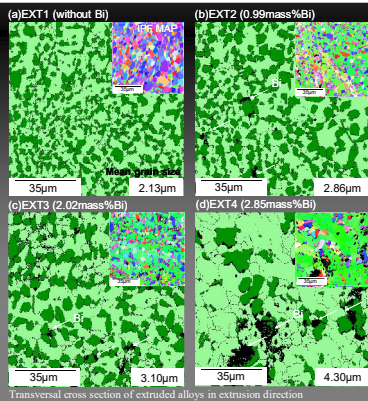
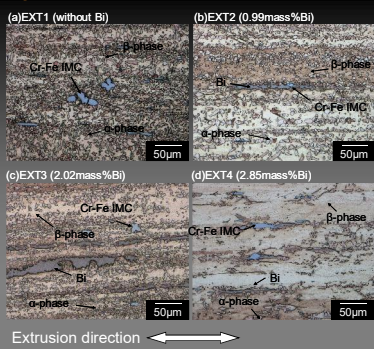


### Optical microstructures

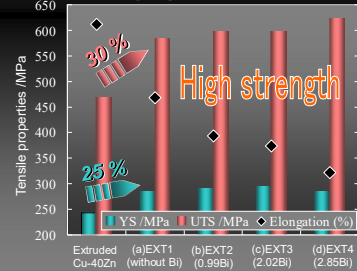
Bi in the  $\beta$ -phase formed spherical particles; however, irregularly-shaped Bi particles formed in or around the  $\alpha$ -phase. The difference in surface tension between Bi particles and the matrix decreased as the elemental Zn content in the matrix increased, and spherical Bi particles then formed in the  $\beta$ -phase which contained higher elemental Zn concentration than the  $\alpha$ -phase.

## Microstructural and mechanical properties of extruded specimens

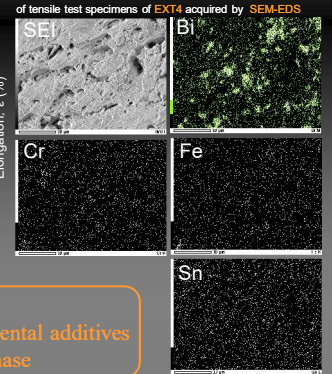
### Optical microstructures



### Tensile properties

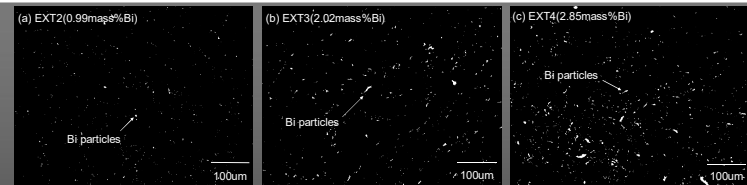


### Fractured surfaces



- The main strengthening mechanism;
- Solid solution strengthening with elemental additives
- Increased area present as the hard  $\beta$ -phase

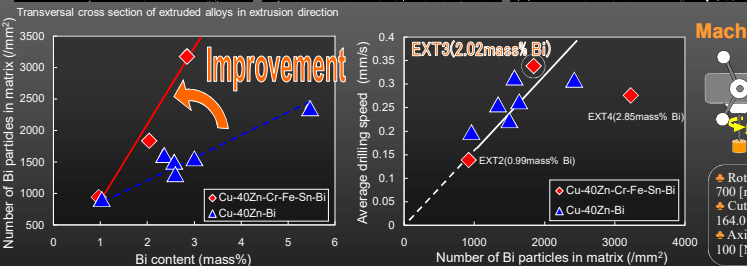
## Relationship between distribution of Bi particles and Machinability



### Back scattered electron images

of EXT2 (0.99mass% Bi) (a), EXT3 (2.02mass% Bi) (b), and EXT4 (2.85mass% Bi) (c) by SEM.

Matrix  
 Bi particles



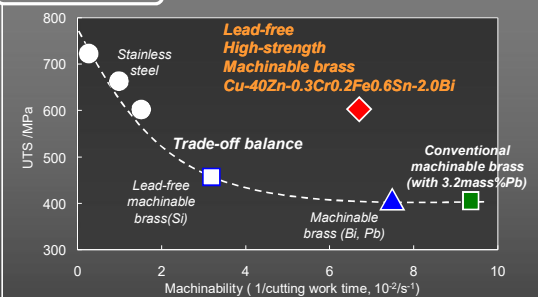
### Machinability test

The drilling time to make a hole with a 5 mm depth was measured; after repeating this drilling test 10 times, the average drilling speed was used as a machinability parameter for the extruded specimens.

- Rotating speed, N 700 [rpm]
- Drill diameter, D 4.5 [mm]
- Cutting speed, V 164.0 [mm/s]
- Drill helix angle 30 [degrees]
- Axial thrust load 100 [N] (10 [kgf])
- Drill point angle 120 [degree]

The extruded Cu-40Zn-Cr-Fe-Sn-Bi alloys exhibited a better dispersion of Bi particles than that of the extruded Cu-40Zn-Pb alloys. Bi morphology in an extruded specimen depends significantly on that of the cast alloy. As above mentioned for the cast alloys, because spherical Bi particles are formed in the  $\beta$ -phase domains, these in  $\beta$ -rich brass become finer than those in  $\alpha$ -rich brass.

## Conclusion



The extruded Cu-40Zn-Cr-Fe-Sn-Bi alloys consisted of  $\alpha$ - $\beta$  duplex phases containing the fine, uniform Cr-Fe IMCs and Bi particles. Average YS and UTS of the extruded Cu-40Zn-Cr-Fe-Sn-Bi alloys were 288 MPa and 601 MPa, respectively. The machinability of the extruded Cu-40Zn-Cr-Fe-Sn-Bi also maintained 75 % of the machinability of a Cu-40Zn-Pb alloy; thus, the extruded Cu-40Zn-Cr-Fe-Sn-Bi deviated from the traditionally observed trade-off between hardness and machinability in conventional machinable brass materials.